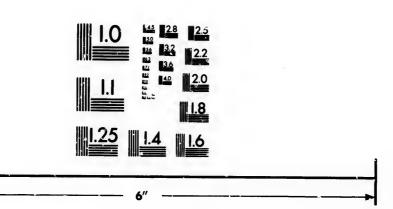


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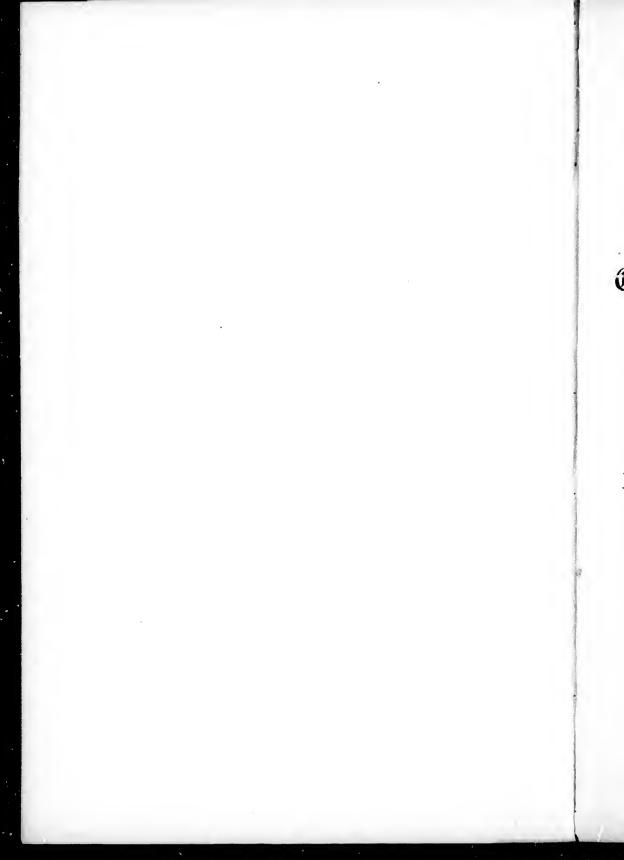
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# REPORT

OF THE

## SURVEY OF EXTENSION

OF THE

European and Horth American Railway

TO THE

# AMERICAN BOUNDARY,

AND

### BRANCH LINE TO FREDERICTON.

BY E. R. BURPEE, C. E.



#### FREDERICTON:

PRINTED BY JOHN GRAHAM, "HEAD QUARTERS" OFFICE. 1865.

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#### PROVINCIAL SECRETARY'S OFFICE,

FREDERICTON, April 27th. 1864.

SIR,

I beg to inform you that his Honor the Administrator of the Government in Council has been pleased to appoint you as Engineer, to explore and Survey a line of Railway from the City of St. John to the Boundary of the State of Maine, via the Douglas Valley; and you are hereby authorised and empowered to employ the necessary Surveyors and Assistants to enable you to prosecute that Survey with all convenient speed.

I have the honor to be,

Sir,

Your obedient servant,

S. L. TILLEY.

E. R. Burpee, Civil Engineer, St. John.

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#### REPORT

OF THE

#### SURVEY OF RAILWAY EXTENSION.

St. John, April 24th, 1864.

TO THE HON. A. H. GILLMOR, PROVINCIAL SECRETARY.

Sir,—Having been previously notified of the appointment confirmed in the foregoing letter, I had, in order that the work should be completed with as little delay as possible, already secured the services of Mr. Thos. Ramsey, long and favorably known as an explorer of experience, had organized a staff, and had made arrangements for a thorough survey, during the summer, of the different routes through Portland and Carleton, to connect with the present line from St. John to Shediac, so that immediately on the receipt of formal instructions, I was enabled to commence work in both directions, and from that time until the last of January of the present year, was fully occupied with the out door work on the main line and a branch to Fredericton. Since, the work on both has been plotted, quantities calculated and estimates of cost prepared, and I am now happy to be able to report that a line has been found, which, although, perhaps, susceptible of improvement, yet presents few engineoring difficulties, can be constructed at a very moderate cost, and traverses a district of country which will produce a remunerative tariff, capable of being largely increased.

General Route of the Line.

The line, shown by the deep red line on the map accompanying the other drawings and this report, starts from the present depot of the European and North American Railway, passes either through Portland to the Suspension Bridge, where it crosses the St. John river, or from the present water terminus extended to harbour line, by means of a ferry, it may connect with some of the lines on Western side and through Carleton, with the main line a short distance West of the bridge. Thence skirting the West shore of South Bay and the St. John river for 16 miles, it reaches the mouth of the Nerepis, and follows its left bank for 8 miles; then leaving that river and crossing the road to Fredericton it enters the Douglas Valley, from which it passes by the North side of Gaspereaux Lake and the valley of the Back Creek, until it crosses the South Branch of the Oromocto river. Thence by a direct course, it crosses the North West Branch of the same river near Hartt's Mills, 43½ miles from St. John;—from which point the branch line to Fredericton diverges. Leaving this place it takes a Westerly course and follows the North West Branch of the Oromocto and its tributary, the Yoho, for some distance. Crossing the latter and two branches of the Lyons' stream, it intersects the main post road between Fredericton and St. Stephen, 26 miles distant from the former, and 53 from the latter place. Thence it reaches the shore of Cranberry Lake, crossing an arm, of which it makes, by a direct line, the outlet of the large Maguaguadavic lake; from thence, bending somewhat to the South, it passes the North side of Mink Lake and Mount Prospect, and crossing the "New Brunswick and Canada Railway" 42 miles from St. Andrews, it reaches the American boundary on the St. Croix river, not far from the outlet of the Cheputneticook lakes, the distance being 881 miles from St. John.

By this route a line has been procured, which requires no grade exceeding 53 feet per mile, or curve of less radius than 1637 feet, and which will be found to compare favorably with most lines on this continent both as to total amount of grades, curvature and cost.

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Characteristic Features of the Line and Works.

Loaving that part of the line East of the Suspension Bridge, and the different means of connecting with the terminus of the European and North American Railway to be afterward considered, I will proceed to remark on the characteristic features of the line from that point Westward, and as there is no very great difference in the length of the terminal lines, it is to be understood that in all cases, where distances from St. John are given, they are reckened from the present depot of the European and North American Railway, and by the line through Portland, over the falls.

From the Suspension Bridge around the South Bay as far as Sutton's Mills the work will not be difficult, but on reaching that point it will be necessary to cut through a spur of limestone rock, 40 feet in depth by 200 feet long, the material can be used to form part of a heavy embrukment required across an arm of the bay. It is also proposed here to erect an iron bridge of 50 feet span, this being the natural outlet of the water from Spruce Lake. Thus far, it is possible to shorten the line at least 1½ miles, and reduce the curvature very considerably, by adopting a line across the South Bay near the line of piers of the Boom Company, but it was found, on examination, that to build a wharf or embankment sufficient to withstand the wash of the water in so exposed a situation, with the necessary bridges and dams, besides interfering with the operations of the Boom Company, would entail an outlay exceeding

that on the longer line, by at least \$100,000.

From South Bay to Vernon's mill pond the work will be light, but thence to Law's stream, the eastern boundary of King's County, a distance of about 3 miles, serious obstacles are to be encountered because of the highlands, which, (skirting the South side of the St. John,) here jut out abruptly into the river, forming Stevens' Cove on the East and Clark's Cove on the West side of Clark's Mount. To avoid a tunnel either through this hill, or the point of high land immediately West of Clark's Cove, which was resorted to in former surveys to overcome the difficulties here met with, much time was spent in a thorough examination of the country for some distance from the river. A practical, and I may add not immoderately expensive line, was found by crossing to the South side of the Fredericton road, (at Stevens'), and recrossing a short distance before reaching Law's stream,—the summit being overcome by a grade of 49 feet per mile, for a distance less than one mile on the Eastern side and about half a mile on the Western side, while the line was generally straight.

A survey and estimate has also been made of an alternative line at this point (shown by a blue line on the plan,) which, passing round the edge of Clark's Point, avoids the summit to be surmounted by the inland route, but being half a mile longer, requiring curves of less radius than 1450 feet, and on

the whole being not less expensive, is not recommended.

For the next 4 miles the country is rough and much broken, so that the work will be necessarily above the average per mile, although the grades are within the prescribed limits and the curvature is moderate. Law's and Scovil's mill streams are each in deep valleys, requiring heavy embankments and bridges of 25 feet span. The highland, extending out into the St. John river at Brandy Point, is passed by taking advantage of a natural valley, most favorably situated, immediately South of that point in a direct line with the general course.

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After this, the ground is much more favorable, and little needing special remark is met with, until reaching the vicinity of Eagle Rock, some distance up the Nerepis and 20½ miles from St. John.

I may here remark, however, that to avoid the necessity of frequently crossing the post road on this section, in order to secure the safety of the travelling

public, a large amount of road diversion will be equired.

At Brundage's Point, 13 miles from St. John, a cutting of 400 feet long and 40 to 50 feet deep is shown on the section, apparently of material suitable for ballast. The existence of a good ballast pit at this point would be highly advantageous, but should the material prove to be not so good as anticipated, the excavation can be diminished by slightly altering the location, which, to a small extent, would increase the curvature.

As the nature of the country at Belyea's, two miles farther on, is such as to admit in location of little choice of ground, considerable expense may be expected in damage to property, but, should the present line, on final location be adhered to, the damage may be considerably reduced, by lessening the width of the cutting and bridging a sufficient portion of it, to allow the proprietor accommodation for his ordinary business. This bridge would also serve for the road leading from this place across the Nerepis river to Brittain's Point.

In the vicinity of Eagle Rock, it will be necessary to encroach slightly upon the Nerepis river, for about 200 feet, where the slope will require to be protected by rip-rap, and probably piling for a very short distance. There will, here also, be a cutting of about 50 feet depth, but as at Brundage's Point, the

material can be advantageously used as ballast.

The line now enters the level country near the junction of the Douglas stream with the Nerepis, crossing the Fredericton road near the residence of Charles Bayard, Esq.; leaving which, with a short curve of 2700 feet radius, it crosses the two branches of the Douglas stream, (each requiring a bridge of 24 feet span,) and enters the Douglas valley. An alternative line is here suggested, (as shown on the plan by the blue line,) which, although adding slightly to the curvature, will cause considerable saving in construction, without injuring the character of the road.

After this, the line skirts the foot of Douglas mountain and the hills on the West side of the valley, avoiding as much as possible the soft ground in the vicinity of Harcourt Lake, and reaches the summit of land between the waters of the Nerepis and Oromocto rivers, 27 miles from St. John, and at an elevation of 171 feet above high tide. The whole of the works on this section are more than ordinarily light, the curvature small, and only once is the maximum

grade of 52.80 feet per mile attained.

Leaving this summit, the line first crosses and then recrosses the back creek, the northern side of which it follows nearly to its mouth; thence in about two miles of straight line it crosses the South Branch of the Oromocto, at the head of tide water, and 40 miles from St. John. The work on a portion of this section is somewhat broken, but not heavy or expensive. Several alternative lines have been run in this distance, but although they reduce the amount of curvature and length of time a little, the necessity for heavier grades and increased expense in construction more than counterbalance these advantages. The crossing of the South Branch of the Oromocto, at a place everyway favorable, is proposed to be effected by an iron girder bridge of 100 feet span; thence to Hartt's mills, on the North West Branch of the Oromocto, the country is level, and consequently the works light, and grades easy.

From this point two lines were presented for consideration. One up the North West Branch of the Oromocto river, and by the South side of the Oro-

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mocto lake, across the Maguaguadavic river to the "New Brunswick and Canada Railway;" the other in a nearly direct West course across the country to the North of that lake through Harvey Settlement, and crossing the Maguaguadavic much nearer its source, to the "New Brunswick and Canada Railway."

From explorations made by parties, under Mr. Wilkinson, in 1850, it seemed quite clear no line could be obtained on the former direction, from the Oromocto lake, across the valley of the Maguaguadavic to the high ground between it and the Digdeguash, without grades exceeding 53 feet per mile, and more than ordinarily heavy work, and it also was evident that the distance must be longer than by the Northern route, while to overcome the necessity for heavy grades and expensive work, by going farther to the South the line would have to be made of even still greater length. I determined, after having had the ridge of highland on the West side and North of the Oromocto lake, (which separate the waters of the Oromocto from those of the Maguaguadavic,) and the valley of the North East Branch of the Maguaguadavic, explored by a small party during the progress of the survey East of Hartt's mills, and having found that a shorter practical line could be had on the North side of the lake, to leave the Southern route to be further examined at some future time should circumstances warrant it, and proceeded with the Northern route.

Having adopted this course, it was necessary to cross the North West Branch of the Oromocto, so soon as a suitable place could be selected. This was found at a very short distance above Hartt's mills, and at a point every way favorable, the width of the valley being contracted and the bed of the stream rock. It is proposed to effect this crossing by means of an iron girder

bridge of two spans of 75 feet each.

After crossing the stream, a table land is soon gained, when a straight and easy line is found up the West side of it for some distance, passing Tracey's mills 47 miles from St. John, and crossing Porcupine Brook near its confluence with the Oromocto, where a heavy embankment of 52,000 cubic yards, and bridge of 24 feet span will be required. Immediately, on leaving this stream, a deep and long cutting occurs, and the maximum grade of 53 feet per mile is required for one mile. It is probable, that by increasing the curvature, so as to cross Porcupine Brook a little farther from its mouth, the summit of land between it and the Yoho could be attained by means of a shorter grade and at less expense.

As the country from this point Westward was a complete wilderness, wholly unexplored and without roads, it was a tedious and somewhat difficult task to decide upon the best route, but after a thorough survey of the Yoho stream, and exploring a large tract of the adjacent country, the line now adopted reaching the Cork Sottlement road 58½ miles from St. John, was found to be the most favorable, the work being under the average, with few and

easy curves and grades generally less than the maximum.

There will be required over the two branches of the Yoho, bridges of 24 feet span.

Leaving this point the greatest difficulties were encountered, requiring a most thorough examination of the country, and it is highly probable that further explorations may furnish improvements in the lines ultimately adopted, or lead to results more satisfactory respecting those which have been abandoned.

From this point, two routes to the "New Brunswick and Canada Railway" again present claims for consideration. The first crossing the Lyons' Stream near its forks; thence by the head of Dead Brook, to what is known as the Long Swamp on the Fredericton and St. Stephen road, (through which it was intended to pass the Harvey Settlement ridge,) and crossing the North East

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Branch and main Maguaguadavic Rivers, and following the head of Davis Brook to the South side of Mount Prospect, it would reach the New Brunswick and Canada Railway about 41 miles from St. Andrews. The second route, following the Lyons' Stream to Cramberry Lake; thence maintaining nearly the same elevation, by keeping as nearly as possible to the head of all the Maguaguadavic waters, and passing on the North side of Mount Prospect, joins the New "Brunswick and Canada Railway," not far from the point at which the former does.

The first mentioned route being the shorter by about 2 miles, was looked upon with much favor, and was not given up until much time had been spent in exploring it, and the lateness of the season rendered it imperative to adopt some one. Although no difficulty was found in getting a good line from the Cork Settlement road to Dead Brock, all our explorations as yet, lead to the conclusion, that to make the summit of the Long Swamp, a grade of 60 feet per mile would be required, which, notwithstanding the work would be light, it is not though fit to recommend. It was also ascertained, after having run a number of trial lines, that neither the valley of the North East nor Main Maguaguadavic Rivers could be crossed, so as to reach the "New Brunswick and Canada Railway" South of Mount Prospect, without steeper grades and much heavier work than would be desirable. Finding then, that both of these streams flow and fall rapidly, while the highland on their banks retains its full height, so that a good line in this direction was not likely to be found without much further exploration, if at all, and considering the season was so far advanced, it was decided to keep, as nearly as possible, the elevation attained at the Cork Settlement, and cross both those streams as near their sources as possible.

This led to the adoption of the Northern or second named route on which for 8 miles two lines have been surveyed as shown on the plans, both of which come within the required limits as to grade and curvature.

That by Cranberry Lake (upon which the estimates are based,) crossing the Harvey Road at an elevation of 55 feet lower than any other can, is shorter by a few feet, is much the straightest and presents the smallest amount of heavy gradients. It traverses a heath for two miles, (some three or four hundred feet of which may require to be covered with poles or bush before a bank is laid thereon,) and then after some distance in a swamp, rises with a grade of 52\frac{3}{4} feet per mile from the head of Lyons' Stream through a gorge, the contracted limits of which will admit of very little alteration on final location, to the Post Road from Fordericton to St. Stephen, at an elevation of 471 feet above tide level.

Leaving the Post Road it immediately traverses a cove of Cranberry Lake, with a curve of 1637 radius passes a point of rock, (which makes out from the Scuthern shore and requires to be excavated to a depth of 45 feet,) and then crossing an arm of the lake 800 feet wide, it rises with an easy grade of 20 feet per mile for 5000 feet to an elevation of 488 feet above high tide, the summit between St. John and the "New Brunswick and Canada Railway." The depth of water in the Lake where the line crosses was found to be 16 feet, and with the material furnished from the rock cutting it would not be difficult to make through it a substantial wharf or embankment. The quantity of rock estimated to be excavated at this point is 40,000 cubic yards, (by far the heaviest cutting on the line,) but by increasing the curvature, the quantity of excavation and also the depth of water can be lessened considerably, while at the same time the requirements of a first class road will be adhered to.

The alternative line shown in blue on the plan runs almost entirely on firm ground, but, as it involves the necessity of an increased number of sharp curves,

a higher summit by 40 feet, and consequently a greater length of heavy grades, without reducing the length or to any considerable extent the cost of the line, it is not recommended.

Leaving Cranberry Lake, the line is straight to the Magnaguadavic river, which it is proposed to cross by an iron girder bridge of 50 feet span. On this length the grades are easy and the work light, while there is little doubt but it can be still further improved on final location. The North-East Branch is crossed near the mouth of Deadwater brock and will require a bridge of 30 feet span.

The Maguaguadavic river is crossed a short distance below the outlet of the big Maguaguadavic Lake, and although approached on either side by a grade of 52½ feet per mile, still requires an embankment of 89,000 cubic yards. The valley through which this river flows is much lower than the lands on either side, which will account for this section being among the most difficult and expensive on the line. This valley widens and its depth increases in descending from the Lake, so that the only chance of finding a more favorable crossing must be confined to the short space between the present location and the Lake, where no doubt, from what examinations have been made, the embankment may be considerably diminished in quantity.

After leaving the valley of the Maguaguadavic the country is much more favorable, and following the location we cross Mink Brook nearly one mile from where it enters the Maguaguadavic Lake, and keeping on the right bank of a lake of the same name at its head, skirting the foot of Oak Mountain until the South fork of the Cranberry Brook is crossed near its source, and then traversing heaths and swamps for two or three miles we reach the vicinity of Mount Prospect. Passing this mountain on the narrow strip of level but stoney land between it and Foster Lake, with a short curve of 5270 feet radius toward the South, we cross the head of White Beaver Brook and without difficulty reach the "New Brunswick and Canada Railway" on the level. On the whole of this distance, 10 miles, the location is almost entirely straight, the grades easy and the work not expensive.

Leaving the railway the line keeps still to the South in order to avoid the hills on the Western shore of the second Digdequash Lake, and at the 84th mile from St. John passes a summit of 500 feet above tide level by 2 miles of the maximum grade, then turning to the right and descending with easy grades reaches the American Boundary at the St. Croix, (88 3.5 miles from St. John,) which river it crosses at an elevation of 381 feet above high tide.

Some portions of the work on this section of the line are heavier than an average of the whole, but there is little doubt it can be made lighter on final location. To effect the crossing of the St. Croix will require an iron bridge of two spans of 80 feet each, the expense of one-half which would necessarily devolve upon the company constructing that portion of the line on the American side of the boundary.

Description of Terminal Lines through Carleton and Portland.

Before entering upon the question of cost, it is deemed preferable to make a few remarks on the different lines connecting with the terminus of the European and North American Railway, and with the waters of St. Jan harbour.

A line tolerably favorable, has been surveyed to the terminus of the E. & N. A. Railway, crossing the St. John river about 150 feet above the bridge. From this, it curves to the left and follows the hillside to the vicinity of the iron works on the Straight Shore, thence crossing the timber ponds and the Straight Shore road near Hawes' Cottage, passing over Sheriff street, under Simonds' street, and following from Acadia street, along the rear of the houses on Main street, (Portland,) it reaches the long wharf and thence commences to

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make a Euroarbour. e E. & bridge. of the under houses ences to curve to the right. Then reversing it passes over Mill-street, and through the wooden buildings attached to Harris' foundry, joining the present railway near Dorchester street crossing. From near the suspension bridge to within 700 feet of the present station, the grade descends at a uniform rate of 35 feet per mile. Bridges will be required over Mill street and the long wharf, under Simonds' street, over the Straight Shore road, and trestle work over a portion of the mill pond. The whole of the excavation required will be rock, and through Portland it is proposed to tunnel 250 feet in length.

This may be considered as favorable a line as can be found to connect with our present railway by the Eastern side of the river, but it is very evident that apart from the bridge over the St. John river the works alone are heavy

and must prove expensive.

With a view, if possible, to obviate this objection as well as to furnish more accommodation for heavy freight and lumber traffic, several others have been surveyed on the Western Side of the river, which are shown on the plan of

the harbour and its vicinity.

The first of these leaves the main line at a point "A" (on the plan) 140 West of the bridge by a sharp curve, and passing through the grounds of the Lunatic Asylum, and a little to the West of Peters' mill, follows the bank of the river to Front Row, in Carleton; thence passes between high and low water mark, crossing two or three wharves and the head of Buttermilk Channel to Navy Island. This is only about 1½ miles in length and is the shortest line from the West to the harbour in deep water. It is, however, liable to some objections. The curves near the Suspension Bridge are only of a radius of 1437 feet, and the elevation of ground at the point where it leaves the main line is such that the maximum grade of one foot per hundred is required to within 700 feet of the terminus in order to make a descent to a level with the wharves, while at the same time the works are both heavy and of an expensive nature.

Another line diverges from this some distance before reaching Front Row, then crossing King and Union streets and the heads of the wharves East of Union street, it extends to deep water at Sand Point. This line is about 800 feet longer than the first, which will admit of some diminution in the inclination and will lessen the quantity of work near the Suspension Bridge, but it is liable to the same objection in respect to curvature and to the short distance

between the foot of the grade and the terminus.

A trial line was run from station 26 on the main line, crossing the Manawagonish road to the back of Clark's house, then recrossing the road and along the slope of the hill below Tilton's to near the back of the Church on King Square, and thence into Lancaster street, as shown by the light red line on the plan.

This was found to be impracticable on account of the height of the land at

the road crossing West of King Square.

It then became quite evident, the only chance of obtaining a more favorable line must be to pass on the West side of Carleton Heights. A line was therefore started from point "B" or station 35, on the main line running through the ridge of land on which is the road to St. Andrews, around the highlands to Negro Point, and thence through Carleton to Tavy Island. As this line is about 2 miles longer than the others it may be a question if its length does not more than compensate for the advantages it possesses in grades, curvature and works. It is, however, certain this line can be carried from Negro Point to deep water at Sand Point with a saving both in distance and expense, while at the same time (should a terminus be made there,) it would assist in forming a

breakwater for the protection of the harbour. And should it be found practicable on examination to carry it through the ridge on the Manawagonish road further to the West, so to connect with the main line near Sutton's mills, it

will compare to advantage with the other lines.

It is pretty certain that the lines through Carleton cannot be departed from to any great degree, but a more extended survey than the time and means at my disposal warranted might furnish information that would improve them and at the same time diminish their cost. Indeed in works of so heavy a nature and likely so sciously to affect the value of property through which they pass, the slightest improvement in location would, in construction, many times re-

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pay the expense of any survey that could be made.

It has been proposed to bridge the harbour from Navy Island to the Round Reefs near Hilyard's wharf, but in order not to prevent the navigation of the St. John river as at present conducted, it would be necessary to attain such an elevation (as shown by the profile plans,) as would prevent a junction with our present railway, except by grades steeper than could be recommended, beside which the cost of the structure and its approaches would probably exceed one million dollars. If, therefore, it should not be deemed expedient at first to erect so expensive a work as a bridge at the Falls to connect through Portland, with the present line, the much more expensive one from Navy Island is out of the question, and there only remains to choose the best line on either side to deep water and connect by ferry.

Terminal Lines on Eastern side St. John Harbour.

Having disposed of the different feasible lines on the West side, it only remains now to discover at what point it is best to obtain access to deep water

on the Eastern side of the harbour from the present railway.

Four distinct plans for doing this have been proposed at different times. One line leaving the railway near the Marsh Bridge passes round the back of the City to the breakwater nearly opposite Sand Point; a second from the present station by a tunnel under the property of the late Judge Chipman to the Market Square; thence by Water street to Reid's Point; a third from the crossing of Mill street, by the head of Union street slip to North Market wharf; and a fourth from the present water terminus across Long and St. Helena wharves to Rankin's wharf

nearly opposite Navy Island.

The line by the Back Shore to the Breakwater was surveyed under the late Chief Engineer of the European and North American Railway, and subsequently, by the City Engineer, and in both cases with a view of its being made applicable as a route to a terminus at the Breakwater. Now, whatever may be its fitness for that purpose, or its claims with a view to extending the business limits of the City and increasing the value of its property, it seems unnecessary to spend time in surveying a line that must be very expensive, when the only object sought was the easiest and safest means of extending our present line of railway Westward.

That the second line through Chipman's Hill, whatever its advantages in location, would be too expensive, is obvious, so that only the third and fourth

remain for consideration.

Of these, the third is the shortest and probably would be the cheapest in construction, but it is a matter of some doubt if sufficient room can be found with-

out interfering too much with the business proper of the place.

The fourth is the most direct and (Navy Island being the terminus on the Western side,) would reduce the width of the ferry to about 1500 feet, over a portion of the harbour as sheltered from corms and as free from currents as could be found on any other practicable route.

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s on the t, over a rrents as Should either of these lines be adopted, there are so many questions involved which do not come within the province of an engineer to decide, that it is impossible for me to more than indicate that either is feasible and can be constructed (damage to property excepted,) at a very moderate expense.

Estimate of Cost.

The cost of the whole line is influenced so much by the location of this terminus, that I have thought it more satisfactory to make an estimate on the cost of the main line from the American Boundary to the Suspension Bridge, and append estimates which at best can only be approximate of the several terminal lines.

The calculations for the quantities in the following estimate are based upon the requirements of a first class road; the width of roadbed on embankments being 18 feet, with a slope of 1½ to 1, and in cuttings from 24 to 30 feet, according to the material, with the same slope; ballast 1 foot for depth under the sleepers, and a rail weighing 63 lbs. to a lineal yard. A fair allowance has been added to the quantities of earthwork for shrinkage, ditches, &c., while the facilities for approaching the line with plant, and the abundance of good building material for the works (in most cases within a few yards,) are such that the prices affixed are supposed to be ample for their performance. The station accommodation is not intended to be of so expensive a character as on the present railway, but is calculated on a liberal scale, for the country traversed, and the equipment estimated would, properly managed, be sufficient to meet the requirements of a larger traffic than I have ever yet calculated upon.

Estimate of the Cost of the Main Line of Railway from the Suspension Bridge at St. John to the American Boundary.

7,500 000000 000000000000000000000000000	. 9 .	
65 miles of clearing at 200 dollars per mile,	\$13,000	
50 miles of fencing at 700 dollars per mile,	35,000	\$48,000
2,020,000 cubic yards earth in embankment, at 25 cents	, 505,000	•
196,400 cubic yards solid rock excavation, at 1 dollar,	196,400-	701,400
Masonry.		
696 cubic yards Ashlar in bridge abutments, at 8 dols.,	5,568	
5,205 cubic yards dry rubble bridge abutments, at 7 dols		
15,710 cubic yards culvert masonry, at 4 dollars,	62,840	
6,000 cubic yards rip rap protection walls, at 1 dollar,	6,000-	110,840
1,010 lineal reds of road diversion, at 2 dollars,	2,020	•
18 public road crossings,	5,750	
100 farm and other crossings,	1,250—	9,020
155 tons Iron girder bridging in place, at 150 dols. per t	on,	23,250
86.74 miles single track, including ballast, sleepers, and		
laying, at 8,000 dollars per mile,	693,920	
5 per cent. additional for sidings,	34,697—	728,617
Land damages on 100 farms, at 100 dollars each,	10,000-	10,000
Stations.		
1 Engine house at terminus,	15,000	
2 Engine houses, intermediate, at 8,000 dollars each,	16,000	
3 principal stations, at 2,500 dollars,	7,500	100
5 second class stations, at 1,000 dollars,	5,000	
10 flag stations, at 300 dollars,	3,000	
8 woodsheds and water tanks, at 400 dollars,	3,200-	49,700
77		00 ===

Engineering and superintendence, at \$1,000 per mile,

Forward,

Forward,		
Rolling Stock.		
10 locomotics, at 10,000 dollars each, 3 snow-ploughs, at 1,000 dollars each, 16 first class passenger cars, at 2,650 dollars each, 8 second class passenger cars, at 1,750 dollars each, 4 baggage and express cars, at 1,500 dollars each, 70 box freight cars, at 700 dollars each, 170 platform cars, at 600 dollars each,	100,000 3,000 42,400 14,000 6,000 49,000 102,000—	316,400
Add for contingencies and unforeseen expenses, 15 per	cent.,	\$2,083,980 312,600
Total,		\$2,396,580

Estimate of Terminal Lines, and Bridge over St. John River.

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The following are approximate estimates of the cost of different terminal lines connecting the main line with deep water and the present line of railway, damages to property apart.

In the estimate for the line through Portland, the most important item of expense is the bridge over the St. John river, which it is proposed to make on the suspension principle, similar to that at Niagara.

The site, about 150 feet above the toll bridge, is very favorable, the rock on which the towers would rest being at considerable elevation above high tide, and presenting every appearance of being well fitted to receive them and the anchorages. The Eastern bank will require excavation, and the Western some embanking, in order to bring the roadway 75 feet above high tide, as required by law, to permit the free navigation of the St. John river. The span will be 620 feet, being longer than any tubular bridge, and about 200 feet shorter than the suspension bridge at Niagara, which answers the double purpose of railway and carriage road. Comparing the natural advantages in the site, the diminution in span, the work it would have to perform, and the facilities for construction with those at Niagara, the conclusion arrived at is that the cost of the proposed structure would not exceed \$200,000.

By crecting abutments from extreme low water on either side, the span can be reduced to 500 feet, at which a tubular or girder bridge would become practicable, and in stiffness and consequent adaptability for rapid transit, might possibly present advantages sufficient to warrant the extra expense required in its construction. From surveys made, an approximate estimate of the cost of both a suspension bridge of 620 feet, and a tubular one of 500 feet span, has been made, and will be found appended to this report.

Estimate of a Line from West side of St. John River, through .  present Line of Railway.	Portland to the
70,000 cubic yards rock excavation, at 1 dollar,	\$70,000
400 lineal feet trestle bridging, at 20 dollars,	8,000
2,600 cubic yards rock excavation in tunnel, at 5 dollars, \$13,00	0
650 cubic yards masonry, lining tunnel, at 8 dollars, 5,20	
Bridges over Mill street, Long Wharf, and two over Straight	e e e e e e e e e e e e e e e e e e e
Shore road,	33,000
Over bridge Simonds street,	1.000
Foregard	

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	1,000 20,000
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	\$351,200
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32,000— 200 400 500— 2,000	\$82,500 1,200 9,000 2,000
	aland and by ailway. \$15,000 6,000 2,000 60,000 60,000 16,000— Ferryboats. 35,000 6,000 40,000 50,000 15,000 16,000 30,000—

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Forward, Bridge over Buttermilk channel, 5 miles superstructure and sidings, Wharfing, &c., on Navy Island,		60,000 40,000 30,000
		\$224,700
Deduct saved on construction of Main	Line.	
80,000 cubic yards earth excavation, at 25 cents, 2,000 cubic yards rock excavation, at 1 dollar, 164 cubic yards culvert masonry, at 4 dollars, 7-10 miles of superstructure, at 8,000 dollars,	\$7,500 2,000 656 5,600—	15,756
		\$208,944
Add for approaches on Eastern side of harbor and ferry-	boats,	91,000
		\$299,944
Estimate for a Line from Negro Point to Sand Poi		Ferry.
30,000 cubic yards of rock excavation, at 1 dollar,	\$30,000 30,000—	\$60,000
120,000 cubic yards of earth excavation, at 25 cents, Culverts,	20,000-	1,500
		1.000
		2,000
Bridge for road to Sand Cove, Crossing Manawagonish road,	300	2,000
Bridge for road to Sand Cove, Crossing Manawagonish road, Crossing extension of Lancaster,	300 300—	2,000
Bridge for road to Sand Cove, Crossing Manawagonish road, Crossing extension of Lancaster, Wharfing, &c., at Sand Point. 4 3-4 miles superstructure,		2,000 600 60,000
Bridge for road to Sand Cove, Crossing Manawagonish road, Crossing extension of Lancaster, Wharfing, &c., at Sand Point,		2,000 60,000 38,000
Bridge for road to Sand Cove, Crossing Manawagonish road, Crossing extension of Lancaster, Wharfing, &c., at Sand Point,	300—	2,000 60,000 38,000
Bridge for road to Sand Cove, Crossing Manawagonish road, Crossing extension of Lancaster, Wharfing, &c., at Sand Point. 4 3-4 miles superstructure,  Deduct saved in construction on Main 30,000 cubic yards earth excavation, at 25 cents,	300— Line. \$7,500	2,000 60,000 38,000
Bridge for road to Sand Cove, Crossing Manawagonish road, Crossing extension of Lancaster, Wharfing, &c., at Sand Point. 4 3-4 miles superstructure,  Deduct saved in construction on Main 30,000 cubic yards earth excavation, at 25 cents, 2,000 cubic yards rock excavation, at 1 dollar,	300— Line. \$7,500 2,000	2,000 60,000 38,000
Bridge for road to Sand Cove, Crossing Manawagonish road, Crossing extension of Lancaster, Wharfing, &c., at Sand Point, 4 3-4 miles superstructure,  Deduct saved in construction on Main 30,000 cubic yards earth excavation, at 25 cents, 2,000 cubic yards rock excavation, at 1 dollar, 134 cubic yards culvert masonry,	300— Line. \$7,500	2,000 600 60,000 38,000 \$162,100
Bridge for road to Sand Cove, Crossing Manawagonish road, Crossing extension of Lancaster, Wharfing, &c., at Sand Point, 4 3-4 miles superstructure,  Deduct saved in construction on Main 30,000 cubic yards earth excavation, at 25 cents, 2,000 cubic yards rock excavation, at 1 dollar, 134 cubic yards culvert masonry,	300— Line. \$7,500 2,000 656	2,000 600 60,000 38,000 \$162,100
Bridge for road to Sand Cove, Crossing Manawagonish road, Crossing extension of Lancaster, Wharfing, &c., at Sand Point, 4 3-4 miles superstructure,	300— Line. \$7,500 2,000 656 5,600—	2,000 600 60,000 38,000 \$162,100

A considerable saving may be made in a line to deep water, by stopping the Carleton Shore line at or near Front Row, and making the level of the terminus or wharves about 20 feet above tide level, in which case the cost, with the necessary hoists for heavy freight, would probably not exceed \$100,000.

It may be remarked here that damage to property, unless borne by the districts respectively traversed, would form on some of the lines a considerable additional charge. The line through Portland will be the most expensive in that respect, while that by Negro Point to Sand Point will be very trifling.

In comparing the merits of a continuous line by bridge over the Falls and through Portland, with that through Carleton and by ferry, it must be remembered that a large additional expense will be continually incurred in running the ferry-boats. It admits of very little doubt but that this expense, and the loss of traffic from detention in transit of passengers and light freight, would much

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Falls and rememning the the loss ild much more than meet the interest on the extra expense required for the construction of a bridge, so as to make the connection with the present railway com-

Estimating, therefore, on a through line from the present railway to the

American boundary, we have the following results:—

861 miles from boundary of the State of Maine to Suspension Bridge, costing, as per estimate, 1 86-100 miles through Portland and over bridge at Falls, as per estimate,

\$2,366,580

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88 6-10 miles,

\$2,747,780

By this estimate it appears the European and North American Railway can be extended to the American boundary, and fully equipped, for \$2,750,000, or a little over \$30,000 per mile. The cost of the New England roads average about \$44,000 per raile, and the present European and North American Railway nearly the same. The Grand Trunk cost about \$40,000, and the Nova Scotia railways about \$50,000, while both of these are inferior in character to the proposed line. After allowing an ample margin for additions usually made in rolling stock on all roads after completion, and which tend to swell the cost of those now in operation, the average of lines on this continent cannot be set

down at much less than \$40,000 per mile.

To show that the difference in the cost of these, and the estimate for Western Extension, is not without reason, it is only necessary to mention a few particulars which tend largely to swell the cost of other roads, but, in this case, are either very small or unknown. Save that, on the first ten miles from the Suspension Bridge, the grading is very light, the country traversed after leaving the St. John river being mostly on the heads of those streams emptying into the Bay of Fundy, causes the amount of bridging to be uncommonly small, lakes and bogs, ordinarily requiring large sums in draining, filling, &c., are almost entirely avoided, and in case of connecting with the European and North American Railway, the outlay for terminal buildings (usually amounting to a large sum per mile,) will not be required.

By a reference to the tables, it will also be seen that the line presents many features highly favorable to its being operated at a moderate cost. The length of curved line is only 25 miles, or little over one-fourth of the whole distance, while but a very small portion of this curved line is on a less radius than 2,900 feet. Of heavy grades, only 14 miles are varying from 45 to 52 3-4 feet per mile, and, of this distance,  $10\frac{1}{2}$  miles descend Eastward, or toward St. John, a result of great importance with reference to the carrying capacity of the road, and in view of the heavy lumber traffic expected in this direction.

Deviations from Route Adopted.

Some deviations from the course adopted, and still within the requirements of a line via the Douglas Valley, being urged at different times, as possessing peculiar advantages, have occupied a portion of my attention, and require some notice here.

Route by South Side of Oromocto Lake.

First among these, I would refer to that, already noticed, up the North-West Branch of the Oromocto river, and by the South side of the Big Oromocto Lake, across the valley of the Maguaguadavic, and by Trout Brook to the St. Andrew's Railway.

It was ascertained during the course of the summer's work, that the level of

the water in the Maguaguadavio and Cheputneticook Lakes differed but little from that of those of the Oromocto and Kedron, and also, that the bed of the Maguaguadavic River fell at the rate of 15 feet per mile after leaving the lake. The distance on the course of the river to the point where it must be crossed by a line South of the Oromocto Lake, was known to be not less than ten miles, while from the shore of the lake it could not be more than three. The conclusions arrived at from this information was, that the obstacles in the way of getting a line in this direction were of a serious nature, but, in order to leave the matter as little doubtful as possible, Mr. Stewart was dispatched with a small party in January last, to trave se and level what was pointed out as being the most favorable ground accessible on both sides the Maguaguadavic.

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This line, as also one run by J. Wilkinson, Esq., C. E., and another by Wm. Mahood, Esq., in 1860, are shown on the General Map, and profiles of each ac-

company the other drawings.

The result of this exploration is as follows:—The Maguaguadavic at this point of crossing is in a deep valley, 220 feet above tide level, while the lake is \$71, and the table land on the West side of the valley 465. As the high ground on the South of the Oromocto Lake extends a considerable distance toward the river, it appears impossible to make the descent without two miles of maximum grade, and work of a very heavy nature. On the West side of the river the ascent may be accomplished by three and half miles of the same grade, and with less expensive works than was at first supposed, but still the distance will be longer and the cost greater than on the adopted line. It has been proposed to carry the line farther toward the South, below the Kedron Lakes, and although by thus increasing the distance the valley of the Maguaguadavic is reached with easier work, yet it is heavier and the grades are steeper in leaving it and gaining the elevation of the high ground to the Westward than would be desirable. In fact, all the information I have been able to gather respecting this country, leads unavoidably to the conclusion that no line can be found here without sacrificing something, either in distance, works, or grades, and this without furnishing any corresponding benefit in traffic.

Spruce Lake Route.

Another deviation from the adopted line has been proposed near St. John. Leaving the Suspension Bridge, and following nearly the course of the St. Andrew's road four miles, it then turns to the right of Spruce Lake, and following the right shore of Menzie's Lake, passing between Belvidere and Nelson Lakes, and to the right of Loch Alva, it joins the adopted line a little below Eagle Rock on the Nerepis, and near the entrance to the Douglas Valley. This line was explored by parties for A. C. Morton, Esq., C. E., in 1853, with a view to avoid the expensive rock cutting and tunnelling on the line following the shore of Grand Bay. By a profile of their survey, which is in my hands, it appears this line would be nearly two miles longer, and though some of the work is not expensive, yet to ascend the high grounds to the North of Spruce Lake, and again make the descent to the valley of the Nerepis, would require steeper grades and more expensive works than any on the adopted line. As this exploration was hasty, and, no doubt, susceptible of improvement, it was at first my intention to have examined this district, with a view to finding a less expensive line than by the river, but having succeeded in avoiding the necessity for tunnelling, and having obtained a line which presents no excessively heavy work, and has more favorable grades than could be hoped for on the Spruce Lake route, I did not consider myself justified in expending the time and money required for its thorough exploration, while the necessity of devoting all the remaining portion of the season fit for such work, to the survey of the Fredericton branch, would have prevented my doing so, had it been deemed advisable. out little ed of the the lake. I crossed en miles, e. The the way order to hed with I out as guadavic.

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at this the lake the high distance hout two Vest side es of the l, but still e. It has • Kedron e Maguarades are the Westen able to at no line works, or fic.

St. John. of the St. , and folnd Nelson tle below ey. This tha view wing the hands, it ne of the of Spruce d require line. As nt, it was ling a less the necesxcessively for on the the time f devoting f the Fredadvisable.

#### FREDERICTON BRANCH.

The survey of this line, made in the months of November and December, 1864, and January, 1865, leaving the main line at the crossing of the North-West Branch of the Oromocto, skirts along between the high ground and freshet level until after passing the Rushagonis River, 10½ miles from Hartt's Mills, thence rises to a summit 105 feet above tide level at Baker's Brook; crossing which it descends with a grade of 53 feet per mile for 5,000 feet, and through a very easy and level country reaches Mill Stream, near its head, and following its left bank on a nearly straight line, with light works, and (with the exception c<sup>c</sup> 3,000 feet of the maximum,) easy grades, approaches the St. John River near Morrison's Mills, and thence, with very easy work and nearly a straight line, enters the town at the rear of the principal streets, and doing little damage to property.

By making the terminus at Odell's Grove, the whole distance is 21½ miles from Hartt's Mills, which is considerab. shorter than the travelled road, and the nearest approach to an air line that I think will be found practicable.

The line was extended to the grounds of the Agricultural Society, which, though adding very little to the cost of the line, is nearly one-half mile longer. The ground in Fredericton, and its immediate vicinity, is so favorable for railway construction that there will be no difficulty in taking the line to any point in it that the necessities of trade, or the interests of the community, may desire.

Of the characteristic features of the work there is very little to be said. As will be seen by reference to the tables appended, the curvature and gradients are both favorable, while the works are more than ordinarily light. An iron bridge of 100 feet span is proposed over the Rushagonis, which, with three small bridges at other points, will cover all demands for that class of work.

This line traversing nearly its entire length through barrens and unimproved land, damages to property, except in the vicinity of Fredericton, will be light.

The following estimate, based upon the requirements of the same class of road as the main line, shows that it can be constructed for \$495,357, or about \$22,000 per mile.

was, oo per mile.		
Estimate of Cost of Fredericton Branch	h Line.	
20 miles of clearing, at 200 dollars,	\$4,000	
213 miles of fencing, at 700 dollars,	15,050-	\$19,050
397,840 cubic yards earth excavation, at 25 cents,	99,460	
5,000 cubic yards rock excavation, at 1 dollar,	5,000	104,460
Masonry.		
472 cubic yards masonry in crumb rubble, at 8 dollars,	3,776	
635 cubic yards masonry in dry rubble, at 6 dollars,	3,810	
2,300 cubic yards masonry, culverts, at 4 dollars,	9,200-	16,786
45 tons iron girder, Rushagonis, at 150 dollars,		6,750
21½ miles superstructure, at 8,000 dollars,	174,000	
5 per cent. for sidings,	8,700-	182,700
Rolling stock, at 8,000 dollars,		88,000
Stations,		8,000
Land damages,		5,000
		\$430,746
Superintendence and contingencies, 15 per cent.,		64,611
		\$495,357

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# APPENDIX.

Estimate for Railway Suspension Bridge, 620 Feet Spa River at Falls.	ın, over S	t. John
1,500 cubic yards masonry in abutments and anchorages,	2,000 8,000	\$40,000
Cables and Suspenders.	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	<b>#10,000</b>
12,000 strands No. 10 wire, 1,000 feet long, 600,000 lbs., at 15 cents,	0,000	
	4,000 2,880 —	96,880
Saddleplates and Anchorage.	,	20,000,
25 tons cast iron, at 80 dollars, 30,200 lbs. anchorage chains, at 12 cents, 600 lineal feet truss, at 20 dollars, 4,800 cubic feet timber in floor girders, at 60 cents, Flooring,	2,000 3,624— 2,000 2,880 1,000	5,624
Stays and painting, Excavation for towers, anchorage, &c.,	2,000	20,880 2,000
Add contingencies,	\$:	165,384 16,538
	\$	181,922
Estimate for Tubular Girder Bridge across St. John River	. 500 Feet	Span.
2,700 cubic yards masonry, at 20 dollars, 1,500 tons iron work in girder, at 150 dollars, Suspension staging, say,		\$54,000 225,000 182,000
	\$4	61,000

880

41250

TABLE OF ALIGNMENT FROM THE SUSPENSION BRIDGE TO THE AMERICAN BOUNDARY.

	7		_		ENGTH OF	LENGTH OF EACH CLASS OF CURVE	S OF CURVE				
from Suspen- Straight sion Bridge Line, in feet.		Magnetic Course.	Curves under 1°.	1° Curve, Radius 5730 feet.	14° Curve, Radius 3820 feet.	2° Curve, Radius 2865 feet.	24° Curve, Radius 2232 feet.	3° Curre, Radius 1910 feet.	34° Curre, Radius 1435 feet.	Whole No. of Degrees in	REMARKS.
	_		FEET.	FEET.	FEET.	FEET.	FEET.	FEET.	FEET.		
-	-		:	:	:	::	:	900		270	
1450 5	550   N	N. 82° W.	:	:	:	:	:	1150	:	34.15	
			:	:	:	:	:	:	:		
	006	N. 474 W.	:	:	:	:	:	:	:		
			:	:	:	:	:	1984	:	59.30	
6800   1316		S. 73 W.	:	:	:	:	:	:	:		
			:	:	:	1200	:	:	:	24	
_	2 006	N. 83 W.	:	:	:	:	:	:	:		
			:	:	:	:	:	1000	:	30	
	350 S	S. 67 W.	:	:	:	:	:	:	:		
11350			:	:	:	:	:	1100	:	33	
00   1250	_	N. 80 W.	:	:	110	:	:	:	:		
				:	2000	:	:	:	:	25	
15900 1300		N. 55 W.	; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;	:		:		:	:		
			:	:	:		1700	:	:	42.30	
19350   1750		N. 12½ W.		:	:	:		:	:		
			1	:				1000	:	30	
00   4750		N. 17 E.	, :	:			:	:	:		
			:	:		2012		:	:	41.30	
28350   1175		N. 25 W.	·· .	:		:		:	:		
				700		:		:	:	7	
00   1950		N. 32 W.	:	:	i	:	0	:	:		
		a II	. :1	:	1 !			2170	:	65	
_	830 8	S. 83 W.	); (1),					:	:	-	
35800		i i	· · · · · · · · · · · · · · · · · · ·	į.				1800	: :	54	
37500		411	1 1.	:				:	1700	59.30	
0000	-			-							

			-			-							-		-			-		on product			_			-	-		-
59.30	26.25		44.36		77	9.1	#	39	3	50.50	,	65	15	\$	48.45	99 45	22.40	39.15		<b>E</b>	- 00	58.15	06	1	20	3	69	3	65
1700		:		:	:	:	:			:	:	:	:	: :	:	:	:			. :	:	:	:	:	:	:	:	: :	
:::	880	:			200	000	000	1300	:	1675		1170	:	: :	1630	:	:,	1310		:	. 1	1270	:	:	:	:	0300		
				:	•:	:	:	:	: :	:	:	:	:	: :	:	:	:			1725	:	:		:	:	:	:	: :	USTG
			2225	:	:	:	:	:		:	:	:	9550		:		0#11				:	:	1100	0011	:	:		: :	
				:	:	:	:	:		:	:	:	:	: :	:	:	:			:	:	:	:	:	:	:	:	: :	
T.				:	:	:	:	:	: :	:	:		:	: :	:	;	:			:	:	:	:	:	:	:	:	: :	
1 1				:	:	:	:	:	: :	:	:	:	:	: :	:	:	:			:	:	:	:		104 90	3337	:	: :	
N. 10½ E.		N. 94 W.	1	N. 35 E.	c	N. %.	W 16 W	01	N. 55 W.		N. 4½ W.	W 201 TV		N. 114 E.		N. 474 W.	W 141 W		N. 50.45 W.		N. 10.45 W.	100	N. 49 W.	W 57 W	N. 21 W.	(	N. 12 W.	N. 71 W.	
2870		350		975	0000	2900	0000	2300	375		830	200	200	170		286	1945	# 010	175	•	400	100	2675	647	CCTT		629	245	

TABLE OF ALIGNMENT FROM THE SUSPENSION BRIDGE TO THE AMERICAN BOUNDAINY .- CONTINUED.

Straight   Magnetic   Machine   1-5 Curves   1-5 Curves				T	LENGTH OF EACH CLASS OF CURVE	EACH CLASS	OF CURVE				
650         N. 32½° W.         FEBT.         FEBT.         FEBT.         FEBT.         FEBT.         FEBT.         FEBT.         FEBT.         T.30           1742         N. 4½ W.         1450         633         150         150           1390         N. 21 E.         730         22.30         25.30           75         N. 13 E.         666         666         20           309         N. 33 E.         2300         69         69           4800         N. 36 W.         350         14         350           7200         N. 34 W.         350         21         700           700         N. 13 W.         350         23         23           1127         N. 36 W.         350         23         23	Distance Length on Suspen- Straigh on Bridge Line in feat.		Curves under 12.	lo Curve, Radius 5730 feet.	14° Curve, Radius 3820 feet.	2° Curve, Radius 2865 feet.	24° Curve, Radius 2232 feet.	Courve, Radius 1910 feet.	34° Curve, Radius 1435 fect.	Whole No. of Degrees in	REMARKS.
650       N. 32½° W.       1450       633         1742       N. 4½ W.       1275       730         1890       N. 21 E.       730       730         75       N. 13 E.       666       666         309       N. 33 E.       933       2300         4800       N. 36 W.       858       700         700       N. 13 W.       350       700         700       N. 13 W.       773         1127       N. 36 W.       700         367       N. 23 W.       773	-		FEET.	FEET.	FEET.	FEET.	FEET.	FEET.	FEET.		٠
650       N. 32½ W.         1742       N. 4½ W.       633         1890       N. 21 E.       730         75       N. 13 E.       1000         4800       N. 38 E.       666         389       N. 22 W.       933         5970       N. 30‡ W.       350         700       N. 13 W.       773         1127       N. 28 W.       773         367       N. 23 W.       773			:	1450	:	:	:	:	:	14.30	
1742       N. 4½ W.       633         1390       N. 21 E.       730         76       N. 13 E.       1000         309       N. 33 E.       666         4800       N. 36 W.       933         5970       N. 30‡ W.       858         7200       N. 34 W.       350         1127       N. 36 W.         367       N. 23 W.		$32\frac{1}{2}$ ° W	•	:	:	:	:	:	:		
1742       N. 42 W.         1390       N. 21 E.         750       N. 43 E.         309       N. 33 E.         4800       N. 36 W.         3889       N. 22 W.         5970       N. 30 W.         700       N. 13 W.         1127       N. 58 W.         367       N. 23 W.		;	:	:	:	:	:	633	:	150	
1330       N. 21 E.       730         780       N. 43 E.       730         309       N. 33 E.       666         4800       N. 36 W.       22300         5970       N. 32 W.       858         5970       N. 34 W.       350         700       N. 13 W.       700         1127       N. 38 W.       733         367       N. 23 W.       733		N. 4½	:	:	:	• 1	:	:	:		
1330       N. 21 E.       730         75       N. 43 E.       1000         309       N. 33 E.       666         308       N. 36 W.       2300         4800       N. 36 W.       858         5970       N. 30‡ W.       350         7200       N. 34 W.       350         700       N. 13 W.       773         1127       N. 23 W.       433			:	:	:	1275	:	:	:	25.30	
780 N. 43 E. 1000 75 N. 13 E. 666 309 N. 33 E. 666 3889 N. 22 W. 858 5970 N. 30‡ W. 350 7200 N. 34 W. 350 7201 N. 36 W. 773 1127 N. 36 W. 700		N. 21	:	:	:	:	:	:	:		
780 N. 43 E. 309 N. 33 E. 4800 N. 36 W. 3889 N. 22 W. 5970 N. 304 W. 700 N. 13 W. 1127 N. 36 W. 367 N. 23 W.	-		:	:	:	:	:	730	:	22	
75 N. 13 E. 1000 309 N. 33 E. 666 3889 N. 22 W. 858 5970 N. 30‡ W. 350 7200 N. 34 W. 350 7127 N. 36 W. 773 367 N. 23 W. 367		N. 43	:	:	:	:	:	:	:		
75       N. 13 E.         309       N. 33 E.         4800       N. 36 W.         3889       N. 22 W.         5970       N. 30‡ W.         7200       N. 34 W.         700       N. 13 W.         1127       N. 36 W.         367       N. 23 W.			:	:	:	:	:	1000	:	30	
309       N. 33 E.       666         4800       N. 36 W.       2300         3889       N. 22 W.       858         5970       N. 30‡ W.       350         700       N. 13 W.       700         1127       N. 36 W.       773         367       N. 23 W.       760		N. 13	:	:	:	:	:	:	:		
309       N. 33 E.         4800       N. 36 W.         983       983         3889       N. 22 W.         5970       N. 30‡ W.         7200       N. 34 W.         700       N. 13 W.         1127       N. 36 W.         367       N. 23 W.			:	:	:	:	:	999	:	20	
4800 N. 36 W. 858 3889 N. 22 W. 858 5970 N. 30 W. 350 7200 N. 34 W. 350 1127 N. 36 W. 773 367 N. 23 W. 23 W.		N. 33	:	:	:	:	:	:	:		
4800 N. 36 W.  3889 N. 22 W.  5970 N. 30 W.  7200 N. 34 W.  7127 N. 36 W.  367 N. 23 W.			:	:	:	:	:	2300	:	69	
3889       N. 22 W.       858         5970       N. 30‡ W.       350         7200       N. 34 W.       700         700       N. 13 W.       773         1127       N. 36 W.       433         367       N. 23 W.       433	_	N. 36	:	:	• (	:	:	:	:		
3889 N. 22 W. 858 5970 N. 30‡ W. 350 7200 N. 34 W. 770 700 N. 13 W. 7773 1127 N. 36 W. 367			:	:	933	:	:	:	:	14	
5970 N. 30‡ W. 350 7200 N. 34 W. 350 700 N. 13 W. 773 1127 N. 36 W. 367	_	N. 22 W	:	• • • • • • • • • • • • • • • • • • • •	:	:	:	:	:		
7200 N. 34 W. 700 N. 13 W. 700 N. 23 W. 703	_			858	:	:	:	:	:	8.35	
7200 N. 34 W. 700 700 N. 13 W. 773 1127 N. 36 W. 433		N. 30F	•	•	:	:	:	:	:		
700 N. 13 W. 1127 N. 36 W. 367 N. 23 W.		;	:	350	:	:	:	:	:	3.30	
700       N. 13 W.         1127       N. 36 W.         367       N. 23 W.		N. 34	:	:	:	:	:		:		
1127 N. 36 W. 367 N. 23 W. 367 N. 23 W.	_	;	:	:	:	:	:	100	:	21	
1127 N. 36 W 433 433		N. 13	:	:	:	:	:	:	:		
367 N. 23 W 433		;	:	:	:		:	773	:	23	
367 N. 23 W 433		N. 36	:	:	:	:	:	• •	:		
N. 23 W.		1	:	:	:	:	:	433	:	T3	
		N. 23	:	:	:	:		:	:	Č	

136700 | 1460 | S. 76 W. ||

					•					
33	: :		: :		 : :	3300	: :			265200
27.30	:	:	:	:	1830	:	:	N. 36 W.	270	261900
1	:	:	:	:		:	:	N. 652 W.	00017	253600
16.30		:				1650	:	VII 000 IV	07950	232450
42.15	:	:	:	2112	:		: :	N. 47 W.	7188	236800
1	:	:	:			•	:	N. 43 W.	3056	221500
17.45	: :	: :		688		: :	: :	N I		218444
33.36	:	:	:	:	:	5504		N. 224 W.	21755	217555
0	:	·:	:	:	:	1000	:	N. 11 E.	0000	195800
	:	:	:	:	•:	:	0000	G II	3026	199436
	:	:	:	:	: <b>'</b>	:	24.0	N. 22 W.	2007	188500
6.30	:	:	:	:	:	650	: 9	W 90 W	0000	181000
	:	:	:	:	:	• • • • • • • • • • • • • • • • • • • •	:	N. 282 W.	001c	170050
က	:	:	:	:	:	300	:	700	-	173300
		:	:	:	:	:	:	N. 25½ W.	006 —	173000
32.30		•				3250	:			172100
70	:	:	:	Occi	:	: :		N. 7 8.	500	168850
2	:	:	:		:	<u>:</u>	:	. H . 42 . H .	2001	168350
42.30	:	1417	:	:	:	:	:		1850	168900
	:	:	:	:	:	:	:	N- 18½ W.	733	163733
36				1800	:	:	:			163000
>	:					: :	:	N. 174 W.	8150	161200
σ	:	:	:	450	:	•				153050
40.30	:	:	:	:	3230	:	:		79.0	152600
	:	:	:	:	. 140	:	:	N .49 W.	1830	148650
25	:	:	:	:	1670	:	:			<b>D</b> 146820
9)	: :	: :		: :	:	:	:	N. 24 W.	3870	145150
80	:	:			4580				_	141280
Transition of the Principles o					130	:	:	S. 76 W.	1460	136700
		,						-	•	
-: 18	:	 :	3240	- :	:	:		=		135240
		:		: :	: :	: :	: :	N. 23 W.	367	132000
13		433	:	:	:	:	0	N. 36 W.	1127	131200
			:	:	:	:	:			1500013

TABLE OF ALIGNMENT FROM THE SUSPENSION BRIDGE TO THE AMERICAN BOUNDARY.—CONTINUED.

				I	ENGTH OF	LENGTH OF EACH CLASS OF CURVE	S OF CURVE				
from Suspen-Sta sion Bridge I	Length of Straight Line, in Feet	Magnetic Course.	Curves under 1°.	1° Curve, Radius 5730 feet.	1g° Curve, Radius 3820 feet.	2° Curve, Radius 2865 feet.	23° Curve, Radius 2292 feet.	3° Curve, Radius 1910 feet.	3½° Curve, Radius 1637 feet.	whole No. of Degrees in Curve.	REMARKS.
			FEET.	FEET.	FEET.	FEET.	FEGT.	FEET.	FEET.		
279000 113	13800	N. 69 W.	:	::	:	:	:	:	:		
280100			:	1100	:	:	:	:	:	11	
	15700	N. 80 W.	:	:	:	:	:	:	:		
			:	009	:	:	:	-:	:	9	
	1600	N. 74 W.	:	:	:	:	:	:	:	(	
			:	3800	:	:	:	:	:	38	
	20175	N. 36 W.	:	:	:	:	:	:	:		
			:	1550	:	:	:	:	:	15.30	
32£050 2	2525	N. 514 W.	:	:	:	:	:	:	:		
327250		1	:	:	:	:	:	1200	:	36	
	2470	N. 154 W.	:	:	:	:	:	:	:		
_		•	:	:	:	:	2480	:	:	82	
333400			:	:	:	:	:	:	1200	42	
	198	S. 60 W.	:	:	:	:	:	:	:		
334585	-				:	:	.186	:	:	24.50	
	34640	S. 843 W.	:	:	:	:	:	:	:		
			:	675	:	:	:	:	:	6.45	
	10600	N. 881 W.	:	:	:	:	:	:	:		
			:	2850	:	:	:	:	:	28.30	
412406 29	29050	S. 63 W.	:	:	:	:	:	:	:		
413200			:	800	:	:	:	:	:	∞	
	0086	S. 71 W.	:	:	:	:	:	:	:		
426400	1		:	3400	:	:	:	:	:	34	
	2400	S. 39 W.	:	:	:		:	:	:	•(	
_			:	:	:	009	:	:	:	77	
_	550	S. 49 W.	:	:	:		:	:	:	ć	
431400				_,	_	1450		_		5%	

431770 | 370 | S. 20 W. II

	28.30	52.30		48		36		49	
: :	: :	:	:	:	:	:	:	:	:
: :	: :	1750	:	1600	:	1200	:	1630	:
: :	: :	:	:	:	:	:	:	:	:
:	1425	:	:	:	:	:	:	:	:
	: :	:	:	:	:	:	:		:
: :	: :	:	:	:	:	:	:	:	:
: :	: :	:	:	:	:	:	:	:	:
S. 81 W.	20	W 707 W	22	1	91	3	69		S. 20 W.
6625	200	10750	200		400		1200		370
	6625 g: 81 W	S. 81 W.	N. 70½ W. 1750	N. 70½ W. S. 81 W.	S. 57 W. 1600 N. 70½ W. 1750 S. 81 W.	S. 57 W.  N. 70½ W.  S. 81 W.	N. 75 W. S. 57 W. N. 70½ W. S. 81 W.	S. 69 W.  N. 75 W. S. 57 W. N. 704 W. S. 81 W.	S. 69 W.  N. 75 W. S. 57 W. N. 704 W. S. 81 W.

 $1\dot{2}$ 

29

:

600

:

S. 49 W.

550

428800 428800 429400 429950 431400

2040

S. 39 W.

2400

TABLE OF GRADIENTS ON THE MAIN LINE FROM SUSPENSION BRIDGE TO THE AMERICAN BOUNDARY.

Distance from Sus- pension B	Length of Grade.	Inclina- tion per 100 Feet.	Inclina- tion per Mile.	Riso in Foot.	Fall in Foet.	Height above Datum.	REMARKS.
01		l I	1	/		100.00	Suspension Rridge
200	200	Level.				100.00	~
3300	3100		26.40	15.50		115.50	
3500	200					115.50	
5700	2200		22.70		9.50	106.00	
7100	1400			i		106.00	
11600	4500	0.80	42.24	İ	36.00	70.00	
13500	1900					70.00	
16300	2800		36.96		19.60	50.40	Sutton's Mills.
17600		Level.	1			50.40	Editor's mins.
19200	1600		21.12		6.40	44.00	
21000	1800					44.00	*
27500	6500		36.96	45.50		89.50	
27700	200					89.50	
31700	4000		47.52	36.00		125.50	
31900	200					125.50	•
36400	4500		47.52	i	40.50		
37000	600				20.00	85.00	
38823	1823		44.88		15.50	69.50	
43900	5077					69.50	
48700	4800		44.88	40.80		110.30	-
49000	300					110.30	Brandy Point.
54600	5600		44.88		47.60		
54900	300					62.70	
56850	1950		11.61	4.30		67.00	
60400	3550		32.75		22.00		• • • • • • • • • • • • • • • • • • • •
61800 <sup>1</sup>	1400					45.00	Brundage's Point.
63000	1200	0.50	26.40		6.00		
69000	6000					39.00	Belyea's
74000	5000		10.56		10.00		
74700	700					29.00	
79700	5000	0.22	11.61	11.00		49.00	
80600	900					40.00	
82200	1600		26.10		8.00	32.00	
98000	13000		10.56	26.00		58.00	
103000	5000	0.74	39.07	37.00		95.00	Eagle Rock.
104500	1500	Level.				95.00	
107966	3466	0.75	39.60	ŀ	26.00		Bayard's.
110000	2034	Level.	i			69.00	
114400	4400	0.60	31.68	26.40		95.40	
119800	5400	Level.				95.40	
121000	1200	0.20	10.56		2.40		
123860	2860					93.00	
134100	10240		44.88	87.00		180.00	
135700		Level.				180.00	
137700	2000		31.68	13.00		193.00	- i-
137900	200					193.00	Summit between Douglas
146300	8400	0.50	26.40l		42.00	151.00	Stream and Oromocto.

E TO THE

ridge

TABLE OF GRADIENTS ON THE MAIN LINE FROM SUSPENSION BRIDGE TO THE AMERICAN BOUNDARY.—Continued.

	.4		AMERIC	AN BUU	NDARY.	-Contin	NUED.
Distance from Sus- pension B	Length of Grade.	Inclina- tion per 100 Feet	Inclina- tion per Mile.	Rise in Feet.	Fall in Feet.	Height above Datum.	REMARKS.
147000	700					151.00	
150000	3000		10.56		6.00	145.00	
152700	2700	Level.				145.00	Gaspereaux. Lake.
158700	6000	0.10	5.28	6.00		151.00	•
159400	700	Level.		1		151.00	
163590	4190		29.00		23.00		
166800	3210					74.00	
179657	12857	0.42	22.17		54.00	74.00	
182600	2943	Level.				57.00	
186000	3400				17.00	57.00	
190200	4200	Level.				80.00	
193600	3400		35.64	23.00		80.00	
194100	500					58.00	
199100	5000		23.23		22.00	58.00	
199300	200					32.00	
202470	3170		43.29		26.00	32.00	S. Branch Oromocto River
205880	3410		10,120		_0.00	45.00	
213100	7220		9.504	13.00		45.00	
217200	4100			30.57		75.75	
219600	2400		00.00	00.01		75.75	
221500	1900		23.76		8.55		
222000	500		20.10		0.00	67.20	Hartt's Mills.
226584	4584		34.32	29.80		97.00	
235154	8570		04.0%	20.00		97.00	1
239000	3846		34.32	25.00		122.00	
242600	3600		04.02	20.00		122.00	
247490	4890		47.52	44.00		166.00	
248500	1010			11.00		166.00	
251833	3333				20.00		
253000	1167				20.00	146.00	
259000	6000	1		45.00		191.00	
260900	1900			40.00		191.00	
263900	3000			9.00	h	200.00	
277400	13500			135.00		335.00	
282476	5076			133.00		335.00	
294200	11724			111.40			
295200	1000			111.40		446.40	
297200	2000			13.60		446.40	
298600	1400			19.60		460.00	
					95.00	460.00	
302600	4000				35.00	424.00	
304000	1400				04.00	425.00	
307200	3200				24.00	401.00	
308400	1200			0.00		401.00	
310200	1800			9.00		410.00	
310400	200				0.00	410.00	
314400	4000				8.00	402.00	
316200				40.00		402.00	
320000	3800	0.50	26.40	19.00		421.00	

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TABLE OF GRADIENTS ON THE MAIN LINE FROM SUSPENSION BRIDGE TO THE AMERICAN BOUNDARY.—Continued.

REMARKS.	bove	Height above	Faii in	Rise in	Inclina- tion per	Inclina-	Longth of	Distance from Sus-
	atum.	Datum.	Feet.	Feet.	Mile.	100 feet.	Grade.	pension B
	25.00	425.0		4.00	16.36	0.31	1300	321300
Iarvey Settlement Road	98.00 Harv	498.0		73.00	47.52	0.90	8112	329412
•	98.00	498.0				Level.	5488	334900
	15.10	515.1		17.10	20.06	0.38	4500	339400
	74.20	474.2	40.90		24.82	0.47	8700	348100
			16.20		31.68	0.60	2700	350800
N. E. Maguaguadavic.	58.00 N.	458.0					1200	352000
8 8		480.0		22.00	34.32	0.65	3385	355385
	30.00	480.0				Level.	3115	358500
			34.00		44.88	0.85	4000	362500
	46.00	446.0					3100	365600
		461.0		15.50	34.32	0.65	2300	367900
•		461.0					100	368000
		1	45.00	1	47.52	0.90	5000	373000
Maguaguadavic River		416.0	19.00		71102	Level.	300	373300
BB		440.3		24.30	47.52	0.90	2700	376000
		440.3		21.00	1,.02	Level.	200	376200
			30.30	}	52.80	1.00	3033	379233
		410.0	00.00		02.00	Level.	567	379800
		415.5		5.50	29.04	0.55	1000	380800
		415.5		0.00	20.01	Level.	300	381100
			11.50		26.40	0.50	2300	383400
Mink Brook.		404.0	11.00		20.10	L evel.	4500	387900
		421.0		17.00	44.88	0.85	2000	389900
		421.0		11.00	11.00	Level.	900	390800
			6.00		31.68	0.60	1000	391800
		415.0	0.00		01.00	Level.	3400	395200
		419.0		4.00	21.12	0.40	1000	396200
		419.0		1.00	21.12	Level.	5100	401300
		431.0		12.06	9.50	0.18	6700	408000
		459.0		27.94	47.52	0.90	3105	411105
		459.0		21.01	11.02	Level.	5897	417000
			12.00	•	26.40	0.50	2400	419400
		447.0	12.00		20.10		1100	420500
		475.0		28.00	44.88	0.85	3300	423800
		475.0		20.00	11.00		400	424200
Ct A. J D	20.00		13.00		26.40	0.50	2600	426800
St. Andrews Railway.		462.00	10.00		20.10		1700	428300
•		529.00		67.00	52.80	1.00	6700	435200
		529.00		000	02.00	Level.		435400
			26.00		31.68	0.50	4333	439733
		503.00	20.00		31.00	Level.	2467	442200
			18.00		41.18	0.78	2300	444500
		485.00	10.00		11.10	Level.	4500	449000
			52.25		50.60	0.95	5500	454500
		432.7	02.20		00.00		1600	456100
		409.78	00.00		52.80		2300	158400

TO THE

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c River.

TABLE OF ALIGNMENT OF FREDERICTON BRANCH RAILWAY.

Railway.

Participate   Participate					1	LENGTH OF EACH CLASS OF CURVE	SACH CLASS	OF CURVE	.:		W.L. ol. W.	
3900         N. 54 E.         FEBT.         FEBT.         FEBT.         FEBT.         FEBT.           4975         N. 36½ E.         3400           1280         N. 55½ E.         1270         1775           1380         N. 47 E.         1850         1850           300         N. 21½ E.         1825         2100           27294         N. 16½ · 3         680         2100           266         N. 45 E.         2100         2900           250         N. 45 E.         2100         2900           2734         N. 15 E.         1025         1900           2732         N. 5.30 W.         1025         1025	Distance om Suspen- on Bridge	Length of Straight Line		Curves under 1°.	Radius 5730 feet.	14° Curve, Radius 3820 feet.	2° Curve, Radius 2865 feet.	2½° Curve, Radius 2292 feet.	3° Curve, Radius 1910 feet.	33° Curve, Radius 1437 feet.	of Of Curre.	REMARES.
3900       N. 54 E.       875       2400         4975       N. 36½ E.       1270       1775         1380       N. 20 E.       1350       1275         1366       N. 47 E.       1325       2100         27294       N. 16½ 'A       2100       2900         266       N. 45 E.       2100       2900         250       N. 45 E.       2100       1900         2734       N. 15 E.       1025       1900         18325       N. 5.30 W       750       1666	in reet.	in reer.		FEET.	FEET.	FEET.	FEET.	FEET.	FEET.	FEET.		
3900       N. 54 E.       875         4975       N. 36½ E.       1270         1280       N. 55½ E.       1350         13025       N. 20 E.       1350         1300       N. 21½ E.       1276         2666       N. 48 E.       2100         27294       N. 16½ T.       2100         1666       N. 45 E.       2100         250       N. 42 W.       1990         2734       N. 15 E.       1025         18325       N. 5.30 W.       1025	2400				:	:	:	:	2400	:	72	
4975       N. 36½ E.       1270         1280       N. 55½ E.       1776         13025       N. 20 E.       1350         1300       N. 21½ E.       1276         2666       N. 48 E.       2100         27294       N. 16½ · 3       680         6860       N. 45 E.       2100         1666       N. 45 E.       2100         250       N. 42 W.       1990         2734       N. 15 E.       1025         18325       N. 5.30 W.       750	6300	3900	54	:	:	:	:	:	:	:		
4975       N. 36½ E.       1270         1280       N. 55½ E.       1775         13025       N. 20 E.       1350         1350       N. 47 E.       1275         2066       N. 48 E.       1325         27294       N. 16½ T.       680         6860       N. 3 E.       680         1666       N. 45 E.       1990         2734       N. 15 E.       1025         18325       N. 5.30 W.       750	7175			•	:	:	875	:	:	:	17.30	
1280       N. 55½ E.       1270         13025       N. 20 E.       1350         1350       N. 47 E.       1275         300       N. 21½ E.       1325         2666       N. 48 E.       2100         27294       N. 16½ T.       680         6860       N. 3 E.       2100         1666       N. 45 E.       2100         250       N. 42 W.       1900         2734       N. 15 E.       1025         18325       N. 5.30 W.       750	2150	4975	361	•	:	:	:	:	:	:		
1280       N. 55½ E.       1775         13025       N. 20 E.       1350         1350       N. 47 E.       1275         300       N. 21½ E.       1325         2666       N. 48 E.       2100         27294       N. 16½ B.       680         6860       N. 3 E.       2100         1666       N. 45 E.       2100         250       N. 42 W.       1900         2734       N. 15 E.       1025         18325       N. 5.30 W.       750	3420			•	:	1270	:	:	:	:	15	
13025       N. 20 E.       1350         1350       N. 47 E.       1275         300       N. 21½ E.       1325         2666       N. 48 E.       2100         27294       N. 16½ · 3       680         6860       N. 3 E.       680         1666       N. 45 E.       2100         2734       N. 15 E.       1900         18325       N. 5.30 W.       1025	4100	1280	553	:	:	:		:	:	:	1	
13025       N. 20 E.       1350         1350       N. 47 E.       1275         300       N. 21½ E.       1325         2666       N. 48 E.       2100         27294       N. 16½ · 3         6860       N. 3 E.       680         1666       N. 45 E.       2200         250       N. 42 W.       1990         2734       N. 15 E.       1900         18325       N. 5.30 W.       750	6475				:	:	1775	:	:	:	35.30	
1350       N. 47 E.       1350         300       N. 21½ E.       1325         2666       N. 48 E.       2100         27294       N. 16½ · 3         6860       N. 3 E.       680         1666       N. 45 E.       2900         250       N. 42 W.       1900         2734       N. 15 E.       1025         18325       N. 5.30 W.       750	9500	13025	20	:	:	:	:	:	:	:		
1350       N. 47 E.       1275         300       N. 21½ E.       1325         2666       N. 48 E.       2100         27294       N. 16½ · 3         6860       N. 3 E.       680         1666       N. 45 E.       2900         250       N. 42 W.       1900         2734       N. 15 E.       1025         18325       N. 5.30 W.       750	0820			:	:	:	1350	:	:	:	77	
300       N. 21½ E.       1275         2666       N. 48 E.       2100         27294       N. 16½ · 3         6860       N. 3 E.       680         1666       N. 45 E.       2900         250       N. 42 W.       1900         2734       N. 15 E.       1025         18325       N. 5.30 W.       750	2200	1350	47	:	:	:	:	:	:	:		
300       N. 21½ E.       1325         2666       N. 48 E.       2100         27294       N. 16½ · ∃       680         6860       N. 3 E.       2100         1666       N. 45 E.       2500         250       N. 42 W.       1900         2734       N. 15 E.       1025         18325       N. 5.30 W.       750	3475			:	:	:	1275	:	:	:	25.30	
2666       N. 48 E.       1325         27294       N. 16½ · ∃       2100         6860       N. 3 E.       2100         1666       N. 45 E.       2500         250       N. 42 W.       1900         2734       N. 15 E.       1025         18325       N. 5.30 W.       750	3775	300	-101	:	:	:	:	:	:	:		
2666       N. 48 E.       2100         27294       N. 16½ · ∃       680         6860       N. 3 E.       2100         1666       N. 45 E.       2500         250       N. 42 W.       1900         2734       N. 15 E.       1025         18325       N. 5.30 W.       750	5100			:	:	:	1325	:	:	:	26.30	
27294 N. 16½ · ∃ 6860 N. 3 E. 1666 N. 45 E. 250 N. 42 W. 2734 N. 15 E. 18325 N. 5.30 W.	9911	5666	48	:	:	:	:	:	:	:		
27294       N. 16½ · ∃         6860       N. 3 E.         1666       N. 45 E.         250       N. 42 W.         2734       N. 15 E.         18325       N. 5.30 W.	9986			:	:	2100	:	:	:	:	31.30	
6860 N. 3 E. 680 1666 N. 45 E. 2100 250 N. 42 W. 2734 N. 15 E. 1900 18325 N. 5.30 W. 750	7160	27294	$16\frac{1}{2}$	:	:	:	:	:	:	:		
6860 N. 3 E. 2100 1666 N. 45 E. 2500 250 N. 42 W. 15 E. 1025 18325 N. 5.30 W. 750	7840			:	:	:	089	:	:	:	13.30	
1666       N. 45 E.       2500         250       N. 42 W.       2500         2734       N. 15 E.       1025         18325       N. 5.30 W.       750	4700	0989	o3	:	:	:	:	:	:	:		
1666       N. 45 E.       2900         250       N. 42 W.       1900         2734       N. 15 E.       1025         18325       N. 5.30 W.       750	0089			:	:	:	2100	:	:	:	57	
250 N. 42 W. 2534 N. 15 E. 1900 18325 N. 5.30 W. 750	8466	1666	45	:	:	:	:	:	:	:	1	
250       N. 42 W.         2734       N. 15 E.         18325       N. 5.30 W.	1366			:	-:	:	:	:	2900	:	200	
2734 N. 15 E. 1900 18325 N. 5.30 W	1616	250	42	:	:	:	:	:	:	:		
18325 N. 5.30 W	3516			:	:	:		:	1900	:	25	
18325 N. 5.30 W 1025	6250	2734	15	:	:	:	:	:	:	:		
18325 N. 5.30 W	7275			:	:	:	1025	:	:	:	20.30	
120	5600	18325	N. 5.30 W.	:	:	:	:	:	:	:		
	6350			:	:	:	120	:	:	:	15	

TABLE OF ALIGNMENT OF FREDERICTON BRANCH RAILWAY.-CONTINUED.

Distance	T			T	ENGTH OF	EACH CLASS	LENGTH OF EACH CLASS OF CURVES.	3.			
from Suspen- Straight sion Bridge Line in feet.	Straight Line in feet.	Magnetic Course.	Curves ander 1°.	lo Curve, Radius 5730 feet.	1½° Curve Radius 3820 feet.	2° Curre, Radius 2865 feet.	2½ Curve, Radius 2292 fect.	3° Curve, Radius 1910 feet.	30½° Curve, Radius 1637 feet.	Whole No. of Degrees in	REMARKS.
			FEET.	FEET.	FEET.	FEET.	FEET.	FEET.	FEET.	curve.	
106800	2		:			450	:			6	
113300	0009	N. 115 W.	:	:	:	1	:	:	:		
114600	000	7	:	:	:	1300	:	:	:	56	
009611	0001	3(\$ W.	:	:	:		:	:	:		
Total,	92125		,		3370	12905		7200			

TABLE OF GRADIENTS ON THE FREDERICTON BRANCH RAILWAY, FROM HARTT'S MILLS TO FREDERICTON.

REMARKS.	Height above Datum.	Fali in Feet.	Riso in Feet.	Inclina- tion per Mile.	Inclina- tion per 100 Feet.	Length of Grade.	Distance from Junction.
Hartt's Mills.	70.00						0
	75.00		5.00	26.40		1000	1000
		37.00		26.40	0.50	7400	8400
	38.00					8900	17300
	42.00		4.00	17.42		1200	18500
	42.00		Į			400	18900
		5.00		8.448	0.16	3125	22025
•	37.00					4175	26200
	45.00		8.00	21.12	0.40	2000	28200
	45.00					200	28400
		7.00		36.96		1000	29400
	38.00					600	30000
	45.00		7.00	36.96	0.70	1000	31000
	45.00				Level.	200	31200
• • • •		7.00		36.96		1000	32200
	38.00					12100	44300
	37.00	1.0		13.20	0.25	400	44700
	37.00					5100	49800
	40.00		3.00	26.40	0.50	600	50400
Rushagonis.	40.00					5100	55500
9	45.00		5.00	26.40	0.50	1000	56500
0	45.00				Level.	3650	60150
	71.00		26.00	35.64	0.675	3850	64000
	108.00		37.00	52.80	1.00	3700	67700
	108.00					4000	71700
	121.50		13.50	44.61	0.845	1600	73300
	121.50				Level.	5000	78300
	133.00		11.50	42.24	0.80	1440	79740
Summit Cutting.	133.00				Level.	260	80000
. 8	82.00	51.00		52.80	1.00	5100	85100
٠.	82.00	- 1				300	85400
•	108.00		26.00	38.00	0.72	3600	89000
	108.00				Level.	200	89200
	99.00	9.00	!	26.40	0.50	1800	91000
	99.00				Level.	2200	93200
	122.70		23.70	39.07	0.74	3200	96400
	89.00	33.70		52.80	1.00	3370	100300
	84.60	4.40		7.00	0.1325	3300	103600
Fredericton.	42.60	42.00	l	30.44		7300	110900
	47.20			7.60		3200	114100

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#### ABSTRACT OF GRADES ON MAIN LINE.

V.	Falling Eastward in Feet.	Falling Westward in Feet.	Total in Feet.
Level.		1	134939
From 0 to 10 feet per mile.	12700	7220	37727
" 10 " 20 " " "	24250	13200	37450
" 20 " 30 " " "	28357	35190	73547
" 30 " 40 " "	40015	31882	71897
" 40 " 45 " "	23510	22223	45733
" 45 " 52.80 " ".	34531	15000	49531
of 52.80 " ".	20200	5333	25533
4. t	193,563	130,048	458,550

#### ABSTRACT OF GRADES, FREDERICTON BRANCH.

	W 1	Falling Eastward in Feet.	Falling Westward in Feet.	Total in Feet.
Level.	10			52915
From 0 to 10 feet per mi	le.	3200	6425	9625
" 10 " 20 " "	(1),131	1200	400	1600
	H1	4600	7400	12000
" 30 " 40 " "	. (	11650	11100	22750
" 40 " 45 " "	11), 11	1600	1440	3040
OI ONICO	n-1, 1 1	3700	8470	12170
	(), () ()	25,950	35,235	114,100

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 $(h_{\mathcal{T}} = -1) \cdot e^{-it}$ 

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otal Feet.

,550

otal Feet.

,100

10,000 1900

